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May 11, 2012

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Mike Monasmith
Senior Project Manager
Systems Assessment & Facility Siting Division
California Energy Commission
1516 Ninth Street, MS-15
Sacramento, CA 95814

| |
|---------------------------|
| DOCKET 11-AFC-2 |
| DATE <u>MAY 11 2012</u> |
| RECD. <u>MAY 14 2012</u> |

Subject: Supplemental Data Response, Set 4
Hidden Hills Solar Electric Generating System (11-AFC-2)

Dear Mr. Monasmith:

On behalf of Hidden Hills Solar I, LLC; and Hidden Hills Solar II, LLC, please find attached a copy of Supplemental Data Response, Set 4.

Hard copies will be sent out to the POS list. Please call me if you have any questions.

Sincerely,
CH2M HILL

John L. Carrier, J.D.
Program Manager

Encl.

c: POS List
Project file

Supplemental Data Response Set 4

Hidden Hills

Solar Electric Generating System

(11-AFC-2)



Application for Certification
Hidden Hills Solar I, LLC; and Hidden Hills Solar II, LLC

May 2012

With Technical Assistance from



Hidden Hills Solar Electric Generating System (HHSEGS)

(11-AFC-2)

**Supplemental Data Response, Set 4
(Responses to Traffic and Transportation, Visual
Resources, and Soil & Water Resources)**

Submitted to the
California Energy Commission

Submitted by
**Hidden Hills Solar I, LLC; and
Hidden Hills Solar II, LLC**

May 11, 2012

With Assistance from
CH2MHILL
2485 Natomas Park Drive
Suite 600
Sacramento, CA 95833

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Figure

DR32-2R2 KOP-7 View from Garnet Road

Attachment

WR3-1 Stormwater Retention Area Maps and Calculations

Introduction

Attached are supplemental responses (Set 4) by Hidden Hills Solar I, LLC, and Hidden Hills Solar II, LLC (collectively, "Applicant") to the California Energy Commission ("CEC") Staff's data requests for the Hidden Hills Solar Electric Generating System project ("HHSEGS" or "project") (11-AFC-2). These materials are in response to questions raised at a workshop held on April 27, 2012, information requested directly by staff (phone or email requests), or additional information that has become known since the AFC was filed.

The responses are grouped by individual discipline or topic area. Within each discipline area, the responses are numbered for tracking and reference convenience. New graphics or tables are numbered in reference to the Supplemental Data Request number. For example, if a table were used in response to Data Request BR-2, it would be numbered Table BR2-1. The first figure used in response to Data Request PD-2 would be Figure PD2-1, and so on.

Additional figures and attachments submitted in response to a data request are found at the end of the Data Responses.

Traffic and Transportation (TT-6)

BACKGROUND

Data Request TT-6 was received by phone from Candace Hill of the California Energy Commission on April 18, 2012.

DATA REQUEST

TT-6. Will any truck traffic to the HHSEGS site travel I-15 coming from the south?

Response: Yes, there will be truck traffic coming from Southern California on I-15 to the HHSEGS site. The trucks will travel I-15 to Las Vegas then head west on State Route 160 to Tecopa Road.

Visual Resources (VR-6)

BACKGROUND

Data Request VR-6 was received by phone conversation with Melissa Mourkas of the California Energy Commission on April 11, 2012.

DATA REQUEST

VR-6. Staff is wondering why KOP 7 only shows one of the two Power Towers. Looking at KOP 7, it seems like if the view had been shifted to the left slightly, two towers would have been shown, as in the original KOP 7.

Response: A copy of the revised KOP 7 simulation (Figure DR32-2R2) is attached. A new base photo, which was obtained from Staff, was used so that both solar towers are visible in this revised simulation.

Soil and Water Resources (WR-3)

BACKGROUND

Data Request WR-3 was received at a workshop held at the California Energy Commission on April 27, 2012.

DATA REQUEST

WR-3. Please provide copies of maps of the stormwater retention area shown to workshop participants on April 27, 2012.

Response: The following resource data, maps and calculations pertaining to the stormwater retention area on the western side of the HHSEGS site (near the Temporary Construction and Laydown Area) are provided in Attachment WR3-1:

- Evaporation Map
- Infiltration Calculations
- NRCS Physical Soil Properties
- Retention Summary
- Retention Area – Initial Ponding
- Retention Area – 24-hr Ponding



A. KOP-7: Existing view toward the project site from Garnet Road, 1.75 miles south of Tecopa Road.



B. KOP-7: Simulated view toward the project site from Garnet Road, 1.75 miles south of Tecopa Road.

FIGURE DR 32-2 R2
KOP-7. View from Garnet Road
Hidden Hills Solar Electric Generating System

Attachment WR3-1
Stormwater Retention Area
Maps and Calculations

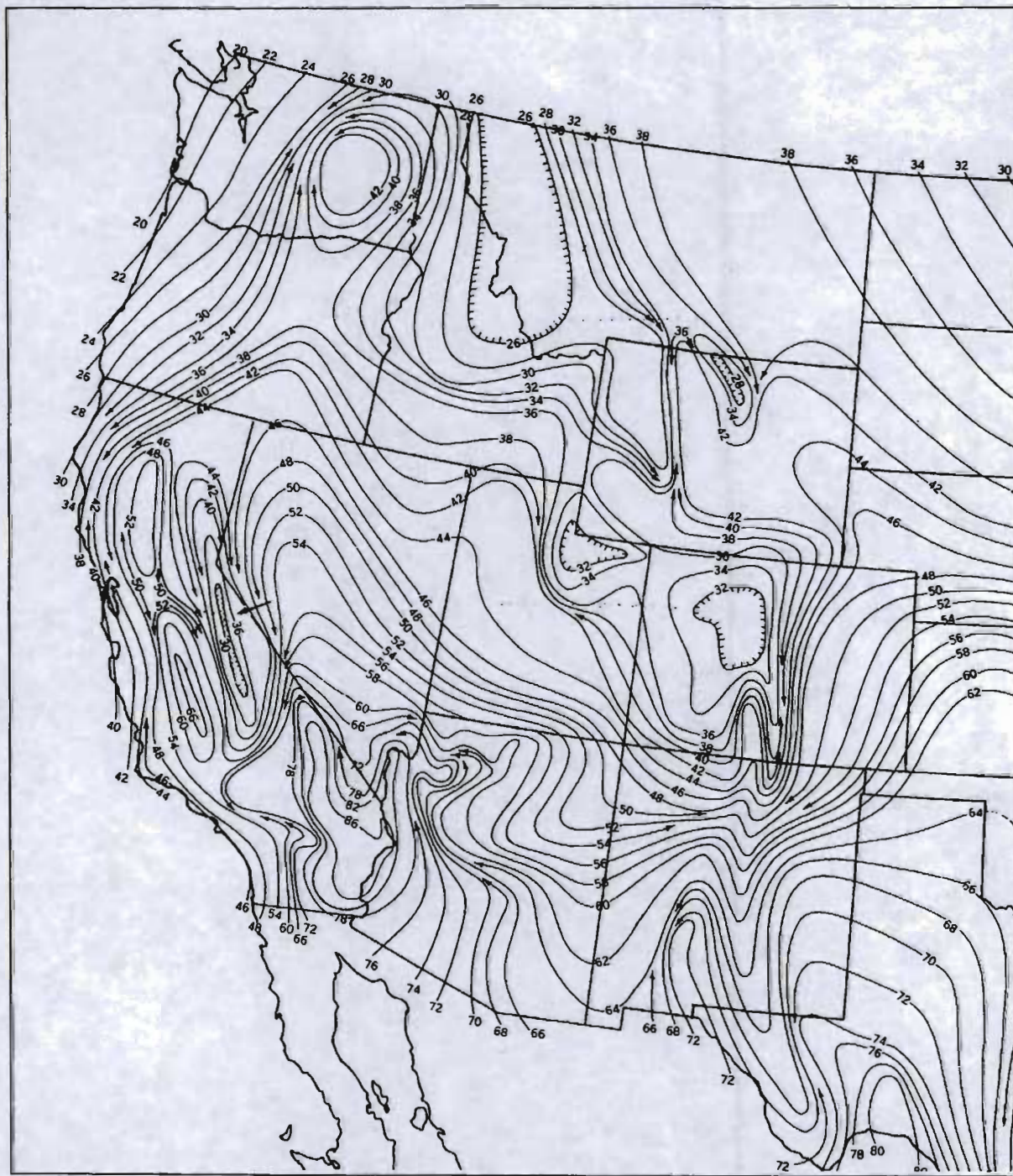


Figure 1.5—Average annual lake evaporation (in inches) in the western United States for the period 1946–1955 (from Kohler et al., 1959, Plate 2).

Soil s5740 Soil Components

Soil Type: Besherm

| Soil Depth (in) | Soil Thickness (in) | Average Hydraulic Conductivity (Micro m/hr) | Average Hydraulic Conductivity (in/hr) | Weighted Average |
|----------------------|---------------------|---|--|------------------|
| 0-2 | 2 | 2.82 | 0.40 | 0.01 |
| 2-60 | 58 | 0.92 | 0.13 | 0.13 |
| Total Thickness = 60 | | | | |

Total Hydraulic Conductivity (in/hr) = 0.14

Soil Type: Nopah

| Soil Depth (in) | Soil Thickness (in) | Average Hydraulic Conductivity (Micro m/hr) | Average Hydraulic Conductivity (in/hr) | Weighted Average |
|----------------------|---------------------|---|--|------------------|
| 0-6 | 6 | 2.82 | 0.40 | 0.04 |
| 6-60 | 54 | 0.92 | 0.13 | 0.12 |
| Total Thickness = 60 | | | | |

Total Hydraulic Conductivity (in/hr) = 0.16

Soil Type: Glencarb

| Soil Depth (in) | Soil Thickness (in) | Average Hydraulic Conductivity (Micro m/hr) | Average Hydraulic Conductivity (in/hr) | Weighted Average |
|----------------------|---------------------|---|--|------------------|
| 0-8 | 8 | 9.17 | 1.30 | 0.17 |
| 8-60 | 52 | 2.82 | 0.40 | 0.35 |
| Total Thickness = 60 | | | | |

Total Hydraulic Conductivity (in/hr) = 0.52

Soil Type: Haymont

| Soil Depth (in) | Soil Thickness (in) | Average Hydraulic Conductivity (Micro m/hr) | Average Hydraulic Conductivity (in/hr) | Weighted Average |
|----------------------|---------------------|---|--|------------------|
| 0-3 | 3 | 9.17 | 1.30 | 0.06 |
| 3-40 | 37 | 9.17 | 1.30 | 0.80 |
| 40-60 | 20 | 9.17 | 1.30 | 0.43 |
| Total Thickness = 60 | | | | |

Total Hydraulic Conductivity (in/hr) = 1.30

Soil Type: Rumpah

| Soil Depth (in) | Soil Thickness (in) | Average Hydraulic Conductivity (Micro m/hr) | Average Hydraulic Conductivity (in/hr) | Weighted Average |
|----------------------|---------------------|---|--|------------------|
| 0-3 | 3 | 0.92 | 0.13 | 0.01 |
| 3-60 | 57 | 0.21 | 0.03 | 0.03 |
| Total Thickness = 60 | | | | |

Total Hydraulic Conductivity (in/hr) = 0.03

Soil Type: Tencee

| Soil Depth (in) | Soil Thickness (in) | Average Hydraulic Conductivity (Micro m/hr) | Average Hydraulic Conductivity (in/hr) | Weighted Average |
|----------------------|---------------------|---|--|------------------|
| 0-2 | 2 | 9.17 | 1.30 | 0.24 |
| 2-11 | 9 | 9.17 | 1.30 | 1.06 |
| Total Thickness = 11 | | | | |

Total Hydraulic Conductivity (in/hr) = 1.30

Soil Type: Bluepoint

| Soil Depth (in) | Soil Thickness (in) | Average Hydraulic Conductivity (Micro m/hr) | Average Hydraulic Conductivity (in/hr) | Weighted Average |
|----------------------|---------------------|---|--|------------------|
| 0-41 | 41 | 91.74 | 13.00 | 8.89 |
| 41-60 | 19 | 28.23 | 4.00 | 1.27 |
| Total Thickness = 60 | | | | |

Total Hydraulic Conductivity (in/hr) = 10.15

Soil Type: Pahrump

| Soil Depth (in) | Soil Thickness (in) | Average Hydraulic Conductivity (Micro m/hr) | Average Hydraulic Conductivity (in/hr) | Weighted Average |
|----------------------|---------------------|---|--|------------------|
| 0-2 | 2 | 28.23 | 4.00 | 0.13 |
| 2-16 | 14 | 9.17 | 1.30 | 0.30 |
| 16-42 | 26 | 2.82 | 0.40 | 0.17 |
| 42-60 | 18 | 9.17 | 1.30 | 0.39 |
| Total Thickness = 60 | | | | |

Total Hydraulic Conductivity (in/hr) = 1.00

Soil Type: Tanazza

| Soil Depth (in) | Soil Thickness (in) | Average Hydraulic Conductivity (Micro m/hr) | Average Hydraulic Conductivity (in/hr) | Weighted Average |
|----------------------|---------------------|---|--|------------------|
| 0-2 | 2 | 9.17 | 1.30 | 0.04 |
| 2-15 | 13 | 2.82 | 0.40 | 0.09 |
| 15-45 | 30 | 2.82 | 0.40 | 0.20 |
| 45-60 | 15 | 70.57 | 10.00 | 2.50 |
| Total Thickness = 60 | | | | |

Total Hydraulic Conductivity (in/hr) = 2.83

Soil Type: Wodavar

| Soil Depth (in) | Soil Thickness (in) | Average Hydraulic Conductivity (Micro m/hr) | Average Hydraulic Conductivity (in/hr) | Weighted Average |
|----------------------|---------------------|---|--|------------------|
| 0-2 | 2 | 28.23 | 4.00 | 0.35 |
| 2-5 | 3 | 9.17 | 1.30 | 0.17 |
| 5-19 | 14 | 9.17 | 1.30 | 0.79 |
| 19-23 | 4 | 0.71 | 0.10 | 0.02 |
| Total Thickness = 23 | | | | |

Total Hydraulic Conductivity (in/hr) = 1.33

| s5740 Soil Type | Soil % | Hydraulic conductivity (in/hr) | Weighted Hydraulic Conductivity |
|-----------------|--------|--------------------------------|---------------------------------|
| Besherm | 25 | 0.14 | 0.03 |
| Nopah | 15 | 0.16 | 0.02 |
| Glencarb | 10 | 0.52 | 0.05 |
| Haymont | 10 | 1.30 | 0.13 |
| Rumpah | 10 | 0.03 | 0.00 |
| Tencee | 10 | 1.30 | 0.13 |
| Bluepoint | 5 | 10.15 | 0.51 |
| Pahrump | 5 | 1.00 | 0.05 |
| Tanazza | 5 | 2.83 | 0.14 |
| Wodavar | 5 | 1.33 | 0.07 |

Hydraulic Conductivity (in/hr) = 1.14

Hydraulic Conductivity (ft/hr) = 0.095

| Storm Event | Ponding Depth (ft) | Infiltration Rate (ft/hr) | Evaporation Rate (ft/hrs) | Infiltration/ Evaporation Drain Time (hrs) |
|-------------|--------------------|---------------------------|---------------------------|--|
| 2-year | 2.79 | 0.095 | 0.0007 | 29.15 |
| 5-year | 3.8 | 0.095 | 0.0007 | 39.70 |
| 10-year | 3.8 | 0.095 | 0.0007 | 39.70 |
| 25-year | 3.8 | 0.095 | 0.0007 | 39.70 |
| 100-year | 3.8 | 0.095 | 0.0007 | 39.70 |

Physical Soil Properties

United States

[Entries under "Erosion Factors--T" apply to the entire profile. Entries under "Wind Erodibility Group" and "Wind Erodibility Index" apply only to the surface layer. Absence of an entry indicates that data were not estimated]

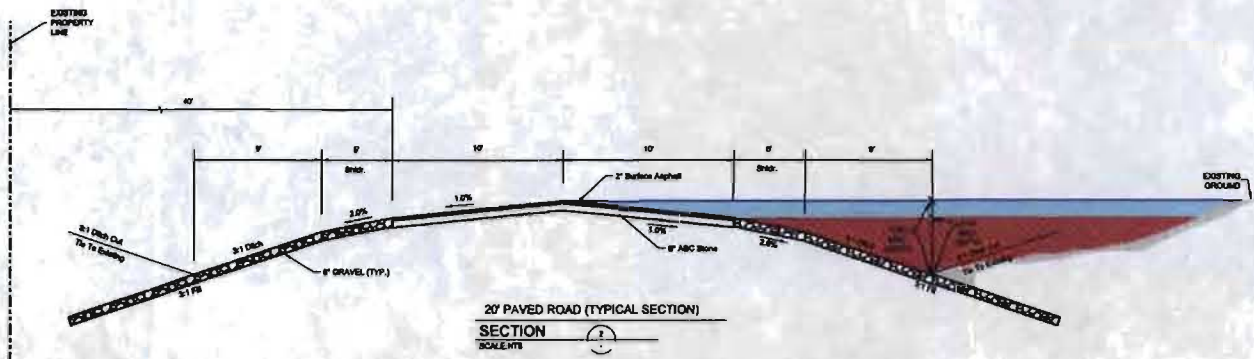
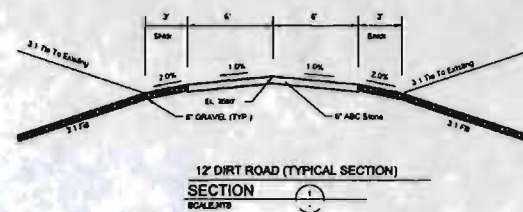
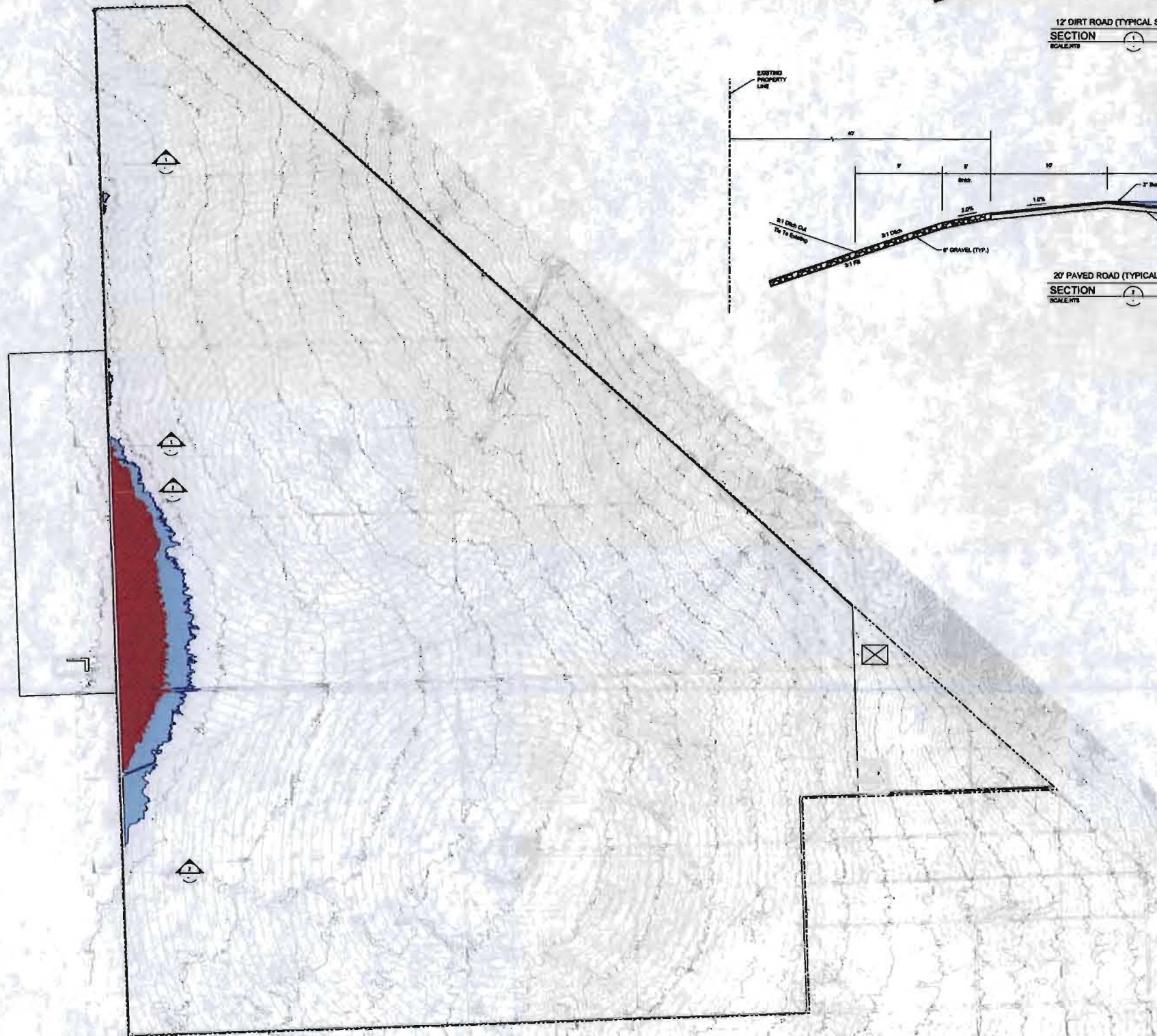
| Map symbol and soil name | Depth | Sand | Silt | Clay | Moist bulk density | Saturated hydraulic conductivity | Available water capacity | Linear extensi- bility | Organic matter | Erosion factors | | | Wind erodi- bility group | Wind erodi- bility index |
|-----------------------------|-------|------|------|-------|--------------------------|--|--------------------------------|------------------------------|-------------------|-----------------|-----|---|-----------------------------------|-----------------------------------|
| | | | | | | | | | | Kw | Kf | T | | |
| | In | Pct | Pct | Pct | g/cc | micro m/sec | In/in | Pct | Pct | | | | | |
| s5740: | | | | | | | | | | | | | | |
| Besherm | 0-2 | --- | --- | 27-40 | 1.35-1.55 | 1.41-4.23 | 0.19-0.21 | 3.0-5.9 | 0.0-0.5 | .32 | .32 | 5 | 6 | --- |
| | 2-11 | --- | --- | 40-60 | 1.30-1.50 | 0.42-1.41 | 0.15-0.17 | 6.0-8.9 | --- | .28 | .28 | | | |
| | 11-60 | --- | --- | 35-50 | 1.30-1.50 | 0.42-1.41 | 0.15-0.17 | 6.0-8.9 | --- | .28 | .28 | | | |
| Nopah | 0-6 | --- | --- | 10-20 | 1.40-1.60 | 1.41-4.23 | 0.16-0.18 | 0.0-2.9 | 0.0-0.5 | .49 | .49 | 5 | 5 | --- |
| | 6-60 | --- | --- | 20-35 | 1.30-1.50 | 0.42-1.41 | 0.19-0.21 | 3.0-5.9 | 0.0-0.5 | .28 | .28 | | | |
| Glencarb | 0-8 | --- | --- | 10-20 | 1.35-1.50 | 4.23-14.11 | 0.19-0.21 | 0.0-2.9 | 0.5-1.0 | .55 | .55 | 5 | 4L | --- |
| | 8-60 | --- | --- | 20-35 | 1.30-1.50 | 1.41-4.23 | 0.18-0.21 | 3.0-5.9 | 0.0-0.5 | .49 | .49 | | | |
| Haymont | 0-3 | --- | --- | 5-15 | 1.35-1.55 | 4.23-14.11 | 0.15-0.17 | 0.0-2.9 | 0.0-0.5 | .43 | .43 | 5 | 3 | --- |
| | 3-40 | --- | --- | 5-18 | 1.35-1.55 | 4.23-14.11 | 0.16-0.18 | 0.0-2.9 | 0.0-0.5 | .37 | .37 | | | |
| | 40-60 | --- | --- | 5-20 | 1.35-1.55 | 4.23-14.11 | 0.16-0.18 | 0.0-2.9 | 0.0-0.5 | .32 | .32 | | | |
| Rumpah | 0-3 | --- | --- | 40-60 | 1.30-1.50 | 0.42-1.41 | 0.14-0.16 | 6.0-8.9 | 0.0-0.5 | .32 | .32 | 5 | 4 | --- |
| | 3-54 | --- | --- | 45-60 | 1.25-1.45 | 0.00-0.42 | 0.14-0.17 | 6.0-8.9 | 0.0-0.5 | .28 | .28 | | | |
| | 54-74 | --- | --- | 40-60 | 1.25-1.45 | 0.00-0.42 | 0.14-0.17 | 6.0-8.9 | 0.0-0.5 | .28 | .28 | | | |
| Tencee | 0-2 | --- | --- | 10-20 | 1.45-1.55 | 4.23-14.11 | 0.15-0.18 | 0.0-2.9 | 0.0-0.5 | .15 | .28 | 1 | 5 | --- |
| | 2-7 | --- | --- | 10-20 | 1.45-1.55 | 4.23-14.11 | 0.05-0.08 | 0.0-2.9 | 0.0-0.5 | .10 | .37 | | | |
| | 7-11 | --- | --- | --- | --- | --- | --- | --- | --- | --- | --- | | | |
| Bluepoint | 0-9 | --- | --- | 2-6 | 1.45-1.65 | 42.34-141.14 | 0.06-0.10 | 0.0-2.9 | 0.0-0.5 | .17 | .17 | 5 | 2 | --- |
| | 9-24 | --- | --- | 2-6 | 1.50-1.65 | 42.34-141.14 | 0.05-0.08 | 0.0-2.9 | --- | .10 | .28 | | | |
| | 24-41 | --- | --- | 2-6 | 1.50-1.65 | 42.34-141.14 | 0.05-0.09 | 0.0-2.9 | --- | .17 | .17 | | | |
| | 41-60 | --- | --- | 2-10 | 1.50-1.65 | 14.11-42.34 | 0.05-0.14 | 0.0-2.9 | --- | .24 | .24 | | | |

Physical Soil Properties

United States

| Map symbol and soil name | Depth | Sand | Silt | Clay | Moist bulk density | Saturated hydraulic conductivity | Available water capacity | Linear extensi- bility | Organic matter | Erosion factors | | | Wind erodi- bility group | Wind erodi- bility index |
|-----------------------------|-----------|------------|------------|------------|--------------------------|--|--------------------------------|------------------------------|-------------------|-----------------|-----|---|-----------------------------------|-----------------------------------|
| | | | | | | | | | | Kw | Kf | T | | |
| | <i>In</i> | <i>Pct</i> | <i>Pct</i> | <i>Pct</i> | <i>g/cc</i> | <i>micro m/sec</i> | <i>In/In</i> | <i>Pct</i> | <i>Pct</i> | | | | | |
| s5740: | | | | | | | | | | | | | | |
| Pahrump | 0-2 | --- | --- | 5-15 | --- | 14.11-42.34 | 0.13-0.15 | 0.0-2.9 | 0.0-0.5 | .32 | .32 | 5 | 3 | --- |
| | 2-16 | --- | --- | 10-15 | --- | 4.23-14.11 | 0.15-0.17 | 0.0-2.9 | --- | .37 | .37 | | | |
| | 16-42 | --- | --- | 20-35 | --- | 1.41-4.23 | 0.08-0.10 | 0.0-2.9 | --- | .15 | .64 | | | |
| | 42-60 | --- | --- | 5-15 | --- | 4.23-14.11 | 0.15-0.17 | 0.0-2.9 | --- | .32 | .32 | | | |
| Tanazza | 0-2 | --- | --- | 5-15 | 1.35-1.55 | 4.23-14.11 | 0.13-0.15 | 0.0-2.9 | 0.0-0.5 | .28 | .32 | 3 | 3 | --- |
| | 2-15 | --- | --- | 15-25 | 1.20-1.40 | 1.41-4.23 | 0.13-0.20 | 3.0-5.9 | --- | .49 | .49 | | | |
| | 15-45 | --- | --- | 25-35 | 1.20-1.40 | 1.41-4.23 | 0.19-0.21 | 3.0-5.9 | --- | .43 | .43 | | | |
| | 45-60 | --- | --- | --- | 1.15-1.35 | 0.00-141.14 | --- | --- | --- | --- | --- | | | |
| Wodavar | 0-2 | --- | --- | 5-10 | 1.30-1.50 | 14.11-42.34 | 0.13-0.15 | 0.0-2.9 | 0.0-0.5 | .28 | .32 | 1 | 3 | --- |
| | 2-5 | --- | --- | 5-18 | 1.25-1.45 | 4.23-14.11 | 0.19-0.20 | 0.0-2.9 | --- | .55 | .55 | | | |
| | 5-19 | --- | --- | 5-18 | 1.15-1.35 | 4.23-14.11 | 0.13-0.20 | 0.0-2.9 | --- | .32 | .32 | | | |
| | 19-23 | --- | --- | --- | --- | 0.00-1.41 | --- | --- | --- | --- | --- | | | |

| | 100-year | 25-year | 10-year | 5-year | 2-year |
|-----------------------------------|----------|---------|---------|---------|---------|
| Peak Flow In (cfs) | 10816 | 4464 | 2091 | 1025 | 44 |
| Peak Flow Out (cfs) | 10771 | 4372 | 2079 | 996 | 0 |
| Peak Volume (acre-ft) | 195.4 | 160.0 | 145.0 | 135.2 | 52.4 |
| Peak Stage (ft) | 2589.41 | 2589.13 | 2589.01 | 2588.90 | 2587.79 |
| Peak Depth of Retained Water (ft) | 3.8 | 3.8 | 3.8 | 3.8 | 2.79 |
| Peak Time (HH:MM) | 2100 | 2035 | 2045 | 2415 | 4705 |
| Retention Amount (acre-ft) | 125.4 | 125.4 | 125.4 | 125.4 | 52.4 |
| Beginning of Overtopping (HH:MM) | 1735 | 1650 | 1650 | 2010 | N/A |
| End of Overtopping (HH:MM) | 6105 | 5035 | 4510 | 4620 | N/A |
| Overtopping Duration (HH:MM) | 4330 | 3345 | 2820 | 2610 | N/A |
| Depth of Overtopping (ft) | 0.61 | 0.23 | 0.21 | 0.1 | N/A |



LEGEND

5, 10, 25, & 100-YEAR STORM EVENT INITIAL PONDING

1-YEAR STORM EVENT INITIAL PONDING

NOTES:

SITE LAYOUT AND CROSS SECTIONS ARE BASED UPON DRAWING: C-2000.DWG DATED MAY 18, 2011, PREPARED BY CH2M HILL.

STORM EVENT CALCULATIONS WERE PREPARED BY VTN AND ARE BASED UPON THE FINAL POST CONSTRUCTION HYDROLOGIC AND HYDRAULIC ANALYSIS DATED JUNE 23, 2011, PREPARED BY VTN, AND THE EXISTING CONDITION HYDROLOGIC AND HYDRAULIC ANALYSIS DATED MAY 24, 2011, PREPARED BY VTN.

RETENTION CALCULATION TABLE

| Storm Event | Initial Ponding Depth (ft) | Initial Pond Elevation | Infiltration Rate (ft/hr) | Evaporation Rate (ft/hr) | Infiltration/ Evaporation After 24 hrs (ft) | 24 hr Ponding Depth (ft) | 24 hr Pond Elevation |
|-------------|----------------------------|------------------------|---------------------------|--------------------------|---|--------------------------|----------------------|
| 2-year | 2.79 | 2587.79 | 0.095 | 0.0007 | 2.30 | 0.49 | 2585.49 |
| 5-year | 3.8 | 2588.8 | 0.095 | 0.0007 | 2.30 | 1.50 | 2586.50 |
| 10-year | 3.8 | 2588.8 | 0.095 | 0.0007 | 2.30 | 1.50 | 2586.50 |
| 25-year | 3.8 | 2588.8 | 0.095 | 0.0007 | 2.30 | 1.50 | 2586.50 |
| 100-year | 3.8 | 2588.8 | 0.095 | 0.0007 | 2.30 | 1.50 | 2586.50 |

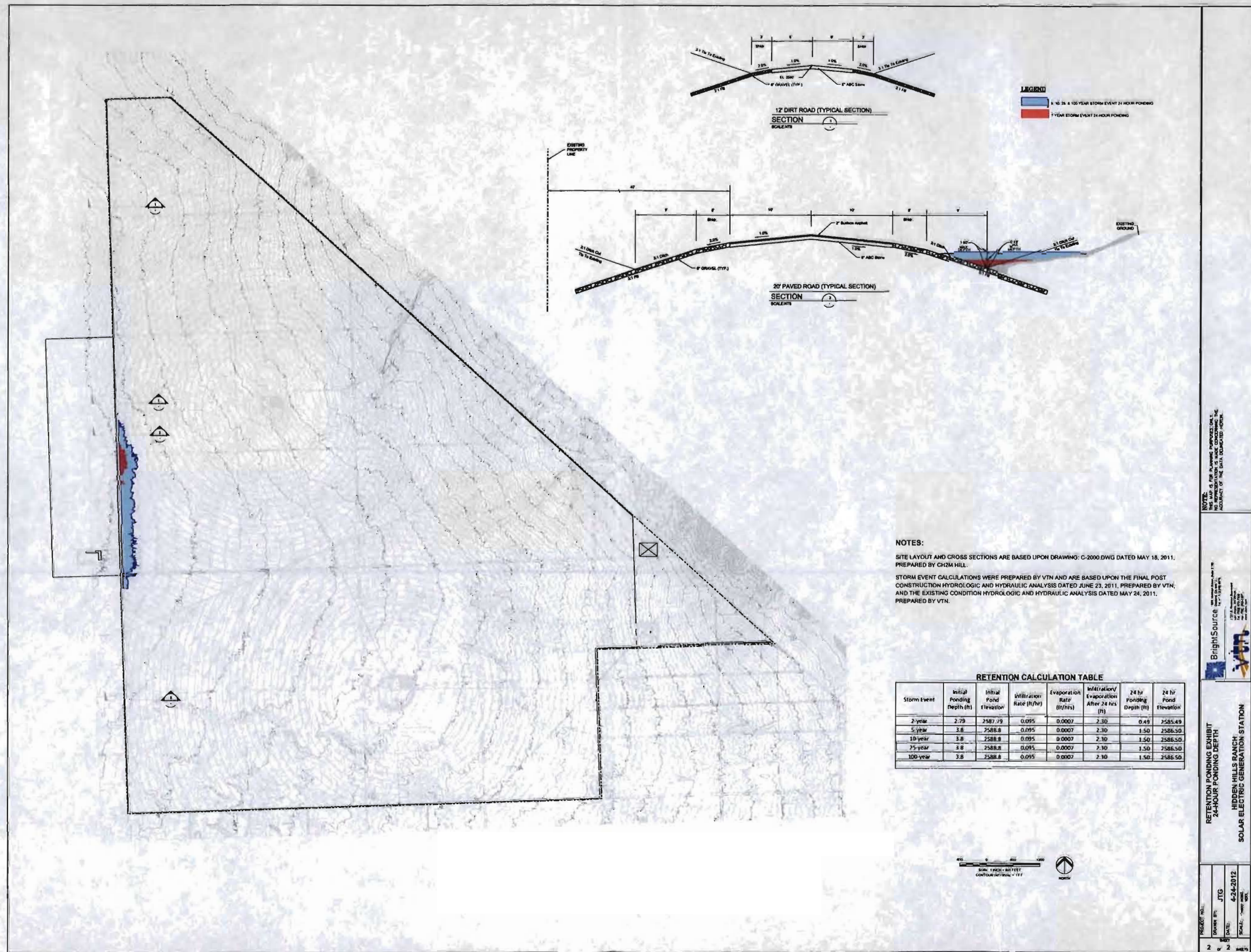


NOTES:
THIS MAP IS FOR PLANNING PURPOSES ONLY.
NO REPRESENTATION IS MADE CONCERNING THE
ACCURACY OF THE DATA DELIVERED HEREON.



RETENTION PONDING EXHIBIT
INITIAL PONDING DEPTH
HIDDEN HILLS RANCH
SOLAR ELECTRIC GENERATION STATION

| | |
|-------------|--------------------|
| PROJECT NO. | JTG |
| DRAWN BY | JTG |
| DATE | 4-24-2012 |
| SCALE | 1"=400' (SEE PLAN) |





**BEFORE THE ENERGY RESOURCES CONSERVATION AND DEVELOPMENT
COMMISSION OF THE STATE OF CALIFORNIA
1516 NINTH STREET, SACRAMENTO, CA 95814
1-800-822-6228 – WWW.ENERGY.CA.GOV**

**APPLICATION FOR CERTIFICATION
FOR THE *HIDDEN HILLS SOLAR ELECTRIC
GENERATING SYSTEM***

DOCKET NO. 11-AFC-02

**PROOF OF SERVICE
(Revised 5/1/2012)**

APPLICANT

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Nye County Water District
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DECLARATION OF SERVICE

I, Mary Finn, declare that on May 11, 2012, I served and filed copies of the attached Hidden Hills Supplemental Data Response, Set 4, dated May 11, 2012. This document is accompanied by the most recent Proof of Service list, located on the web page for this project at: www.energy.ca.gov/sitingcases/hiddenhills/index.html.

The document has been sent to the other parties in this proceeding (as shown on the Proof of Service list) and to the Commission's Docket Unit or Chief Counsel, as appropriate, in the following manner:

(Check all that Apply)

For service to all other parties:

- ☐ Served electronically to all e-mail addresses on the Proof of Service list;
- ☒ Served by delivering on this date, either personally, or for mailing with the U.S. Postal Service with first-class postage thereon fully prepaid, to the name and address of the person served, for mailing that same day in the ordinary course of business; that the envelope was sealed and placed for collection and mailing on that date to those addresses **NOT** marked "e-mail preferred."

AND

For filing with the Docket Unit at the Energy Commission:

- ☐ by sending an electronic copy to the e-mail address below (preferred method); **OR**
- ☒ by depositing an original and 12 paper copies in the mail with the U.S. Postal Service with first class postage thereon fully prepaid, as follows:

CALIFORNIA ENERGY COMMISSION – DOCKET UNIT

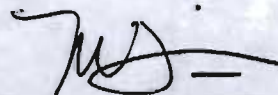
Attn: Docket No. 11-AFC-2
1516 Ninth Street, MS-4
Sacramento, CA 95814-5512
docket@energy.state.ca.us

OR, if filing a Petition for Reconsideration of Decision or Order pursuant to Title 20, § 1720:

- ☐ Served by delivering on this date one electronic copy by e-mail, and an original paper copy to the Chief Counsel at the following address, either personally, or for mailing with the U.S. Postal Service with first class postage thereon fully prepaid:

California Energy Commission
Michael J. Levy, Chief Counsel
1516 Ninth Street MS-14
Sacramento, CA 95814
mlevy@energy.state.ca.us

I declare under penalty of perjury under the laws of the State of California that the foregoing is true and correct, that I am employed in the county where this mailing occurred, and that I am over the age of 18 years and not a party to the proceeding.



Mary Finn, CH2M Hill